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**“YASHIL ENERGETIKA VA UNING QISHLOQ VA SUV XO‘JALIGIDAGI
O‘RNI” MAVZUSIDAGI XALQARO ILMIY VA ILMIY-TEXNIKAVIY
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QOVUSHQOQ-ELASTIK MUHITDA JOYLASHGAN SUYUQLIKLI SILINDRIK INSHOOTLARDAGI GARMONIK TO'LQINLAR YUKLANISHINI TAHLILI

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Annotatsiya. Elastiklik tizimda silindrik ichki yuzasining doiraviy halqasini bir xil turdagi garmonik yuklanganda elastik to'lqinlarning tarqalish masalasi qo'yiladi. Siljish maydoni kontur integrallari sifatida namoyon bo'ladi. Ichki yuzasidagi tebranishlar va to'lqinlar tahlil qilinadi. Uzoqdagi maydon uchun siljishlar va kuchlanishlar uchun yetarli nuqta uslubi bilan asinxronik ifodalar olingan.

Kalit so'zlar: Qovushqoq-elastik muhit, elastik to'lqin, silindrik quduq, seysmik to'lqin.

Abstract. The problem of propagation of elastic waves when a circular ring of the cylindrical inner surface is subjected to a uniform harmonic load an elastic system is posed. The displacement field is represented as contour integrals. The vibrations and waves on the inner surface are analyzed. Asynchronous expressions for the displacements and stresses for the far field are obtained using the sufficient point method.

Keywords: Viscoelastic medium, elastic wave, cylindrical well, seismic wave.

Абстрактный. В упругой системе рассматривается задача распространения упругих волн при воздействии равномерной гармонической нагрузки на круговое кольцо внутренней поверхности цилиндра. Поле смещения выражается в виде контурных интегралов. Анализируются вибрации и волны на внутренней поверхности. Асинхронные выражения для смещений и напряжений в дальней зоне были получены с помощью метода достаточной точки.

Ключевые слова: Вязкоупругая среда, упругая волна, цилиндрическая скважина, сейсмическая волна.

Yer qimirlash jarayonida manba energiyasining ma'lum qismi seysmik to'lbilan birga bo'ladi. Agar yer qimirlash manbai ancha chuqurlikda bo'lsa, u holda yer osti inshootiga birinchi bo'lib bo'ylama to'lyetib keladi, faqat ma'lum vaqt kechikish bilan ko'ndalang to'lkkeladi. Ularni inshootlarga yetib borishi gruntning fizik-mexanik xossalari, to'lgenergiyasi va uning parametrlariga bog'liq bo'ladi. Asosiy massa to'lgeneriyasi ko'ndalang hajmiy to'lbilan tarqaladi. Yetarlicha uzun quvurlar uchun to'lyuklanishini quvurning o'qiga perpendikulyar deb, qo'yilgan masalani tekis masalaga olib kelish mumkbo'ladi. Ko'ndalang to'lginning tenglamadan kelib chiquvchi ($E_1 = E_2, \rho_1 = \rho_2, \nu_1 = \nu_2, \varphi_0 = 0$) halqa (yoki kontur) kuchlanishi ($\sigma_{\theta\theta}^* = \sigma_{\theta\theta} / \sigma_0$; $\sigma_0 = \mu\beta^2\psi_0$; ψ_0 - tushadigan to'lgamplitudasi, μ -Lame koefitsienti)

$$\sigma_{\theta\theta}^* = \frac{8}{\pi} \left(1 - \frac{1}{n^2}\right) \sum_{n=1}^{\infty} i^n \frac{n \left(n^2 - 1 - \frac{\beta^2 \alpha^2}{2}\right) H_n(\alpha a)}{\Delta_n} \sin n \theta e^{-i\omega t}$$

bunda

$$\Delta_n = \alpha a H_{n-1}(\alpha a) \left[(n^2 - 1) \beta a H_{n-1}(\beta a) - (n^3 - n + \frac{1}{2} \beta^2 \alpha^2) H_n(\beta a) \right] + \\ + H_n(\alpha a) \left[-(n^3 - n + \frac{1}{2} \beta^2 \alpha^2) \beta a H_{n-1}(\beta a) + (n^2 - n - \frac{1}{4} \beta^2 \alpha^2) \beta^2 \alpha^2 H_n(\beta a) \right]$$

bunda $\alpha = \frac{\omega}{\sqrt{C_p^2 - i\Delta_p}}, \beta^2 = \frac{\omega^2}{\sqrt{C_s^2 - i\Delta_s}},$

$$\Delta_s = \frac{\lambda_0}{\rho} i (\Gamma_\lambda^c(\omega) + \Gamma_\lambda^s(\omega)), \Delta_p = \frac{\lambda_0}{\rho} i (\Gamma_\lambda^c(\omega) + \Gamma_\lambda^s(\omega)) + 2 \frac{\mu_0}{\rho} i (\Gamma_\mu^c(\omega) + \Gamma_\mu^s(\omega)),$$

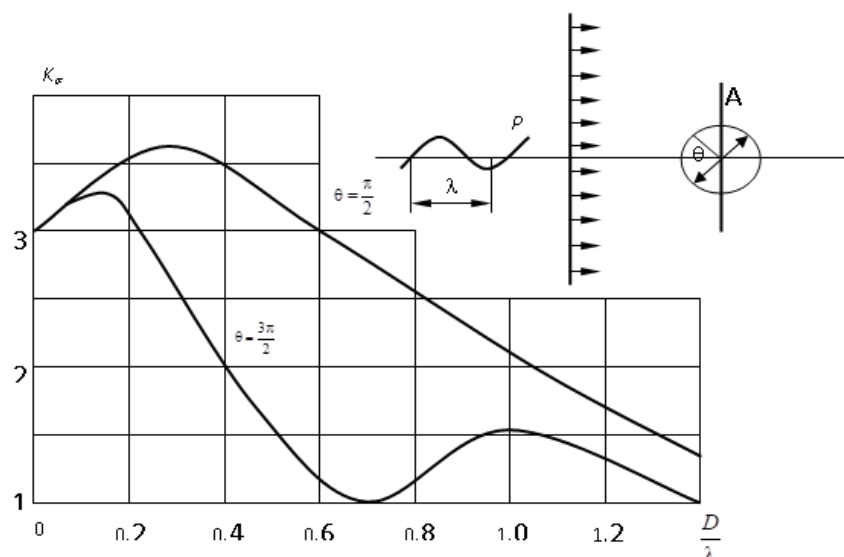
$H_n(\beta a)$ -Xankelning 1-chi jinsli funksiyasi; C_p va C_s -mos ravishda bo'ylama va ko'ndalang to'lgtezliklari; Δ_p va Δ_s -mos ravishda bo'ylama va ko'ndalang to'lginlarni so'nishini ifodalovchi parametr; ω -aylanma chastota, $\pi = 3,14$. Agar to'lguzunligi cheksizlika intilsa va reologik parametrlar nolga intilsa, u holda eng katta qiymatga ega bo'lgan halqa kuchlanishi quyidagicha bo'ladi:

$$\sigma_{\theta\theta} = \frac{2Gv_0}{c_s} (1 - c_s^2/c_p^2) \sin 2\theta \sin \omega t,$$

bunda G -gruntning siljish moduli, v_0 -tushadigan seysmik to'lgamplitudasi. Seysmik to'lginlar uzunligi quvur ko'ndalang kesim o'lchamlaridan katta bo'lganligi sababli $\frac{D}{\lambda} < 1$ bo'ladi. Kuchlanishlarning dinamik konsentratsiyasi koefitsienti K_σ (maksimal halqa kuchlanishini tushadigan to'lgamplitudasiga nisbati) 5.1-rasmda keltirilgan.

Uzun to'lgsohasida ($\frac{D}{\lambda} = 0,04 \div 0,16$) dinamik kuchlanishlar konsentratsiyasi koefitsienti 5-10% statik kuchlanishdan katta ekan [1]. Agar $\frac{D}{\lambda} > 0,16$ bo'lganda dinamik kuchlanishlar konsentratsiyasi koefitsienti statik holat kuchlanishlardan kichik bo'lar ekan. Sonli natijalar 1- va 2- rasmlarda keltirilgan.

Silindrik bo'shliqdagi maksimal kuchlanishlarni paydo bo'lishi, oldingi bobda topilgan diskret chastotalarni mavjudligi bilan izohlanadi. Qovushqoqlik hususiyatlarini hisobga olish dinamik kuchlanishlar konsentratsiyasi koefitsientini 10-15% kamaytirishga imkon beradi. Uzun to'lginli sohada ideal suyuqlikli va suyuqliksiz quvur kuchlanishlari 15%-gacha, qisqa to'lginli sohada esa ularning farqi 40 %- gacha farq qilar ekan.

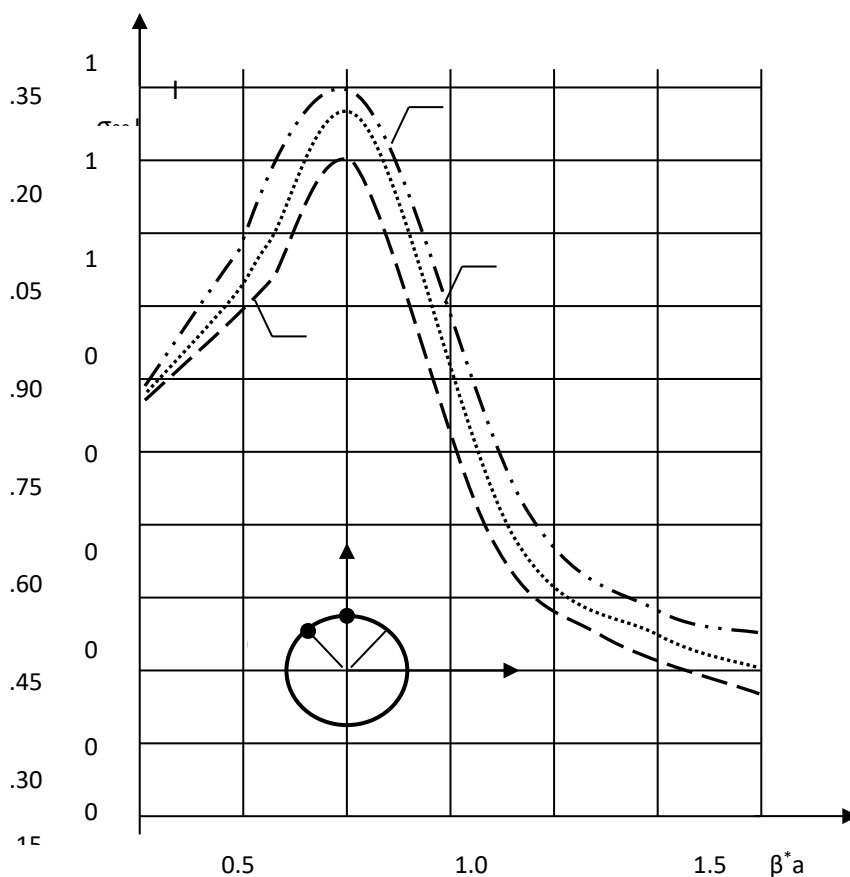


1- **rasm.** Dinamik kuchlanishlar konsentratsiyasi koeffitsienti to'liq uzunligiga nisbatan o'zgarishi.

Agar silindrik jism absolyut qattiq deb olinsa, u holda tekis to'liq bo'yicha olingan natijalar (to'liq uzunligi cheksizga intilsa) quvurning statik holati uchun olingan natijalari bilan ustma-ust tushar ekan [1]

$$\lim_{\beta \rightarrow 0} \sigma_{\theta\theta}^* = -4 \sin 2\theta.$$

Agar qatlam va muhitning xarakterlovchi parametrlar (Yung modullari, Puasson koeffitsientlari va zichliklari) teng bo'lsa va yopishqoqlik xossasi hisobga olinmasa, u holda $r = a$ halqa kuchlanishining $\sigma_{\theta\theta}^* = \sigma_{\theta\theta} / \sigma_0$; $y_0 = \mu\beta^2\psi_0$ ifodasi quyidagi ko'rinishni egallaydi:



2-**rasm.** Halqa kuchlanishini ko'ndalang to'liq soniga nisbatan o'zgarishi.

$$\sigma_{\theta\theta}^* = -\frac{8}{\pi} \left(1 - \frac{1}{k^2}\right) \sum_{n=1}^{\infty} i^{n+1} \frac{n \left(n^2 - 1 - \frac{\beta^2 \alpha^2}{2}\right) H_n(\alpha a)}{\Delta_n} \cdot \sin n\theta,$$

bunda $k^2 = \beta^2 / \alpha^2 = \frac{c_\alpha^2}{c_\beta^2} = \frac{2(1-\nu)}{1-2\nu}$; ν -Puaason koeffitsienti;

$$\Delta_n = \beta^2 \alpha^2 \left(n^2 + n - \frac{\beta^2 \alpha^2}{4} \right) H_n(\alpha a) H_n(\beta a) + \alpha \beta a^2 (n^2 - 1) H_{n-1}(\alpha a) \times \\ H_{n-1}(\beta a) + \left(n - n^3 - \frac{\beta^2 \alpha^2}{2} \right) [\beta a H_n(\alpha a) H_{n-1}(\beta a) + \alpha a H_{n-1}(\alpha a) H_n(\beta a)].$$

Barcha kuchlanishlar va ko‘chishlar quyidagi ko‘rinishda olindi:

$$\left(R + i \operatorname{Im}(lm)^{-i\omega t} (R^2 + \operatorname{Im}^2)^{1/2} e^{-i(\omega t - \gamma)} \right).$$

1-elastik muhit ($A=0$). 2- $A=0,01$; $\beta=0,05$; $\nu=0,25$; $\alpha=0,1$. 3- $A=0,05$; $\beta=0,01$; $\nu=0,25$; $\alpha=0,1$

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